

BUH313

HIGH VOLTAGE FASTSWITCHING NPN POWER TRANSISTOR

- SGS-THOMSON PREFERRED SALESTYPE
- HIGH VOLTAGE CAPABILITY
- U.L. RECOGNISED ISOWATT218 PACKAGE (U.L. FILE # E81734 (N)).

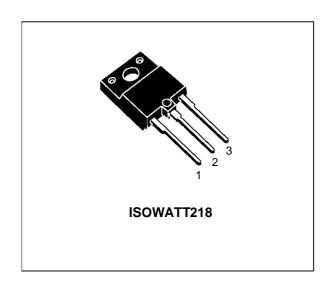
APPLICATIONS:

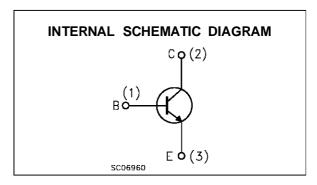
- HORIZONTAL DEFLECTION FOR COLOUR TV
- SWITCH MODE POWER SUPPLIES



The BUH313 is manufactured using Multiepitaxial Mesa technology for cost-effective high performance and uses a Hollow Emitter structure to enhance switching speeds.

The BUH series is designed for use in horizontal deflection circuits in televisions and monitors.





ABSOLUTE MAXIMUM RATINGS

Symbol	Parameter	Value	Unit
V _{CBO}	Collector-Base Voltage (I _E = 0)	1300	V
V_{CEO}	Collector-Emitter Voltage (I _B = 0)	600	V
V_{EBO}	Emitter-Base Voltage (I _C = 0)	10	V
Ic	Collector Current	5	Α
I _{CM}	Collector Peak Current (tp < 5 ms)	8	Α
I_{B}	Base Current	3	Α
I _{BM}	Base Peak Current (t _p < 5 ms)	5	Α
P _{tot}	Total Dissipation at T _c = 25 °C	44	W
T _{stg}	Storage Temperature	-65 to 150	°C
Tj	Max. Operating Junction Temperature	150	°C

June 1996 1/7

THERMAL DATA

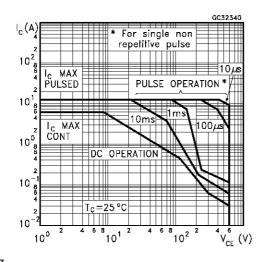
R _{thj-case}	Thermal Resistance Junction-case	Max	2.8	°C/W	
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ELECTRICAL CHARACTERISTICS (T_{case} = 25 °C unless otherwise specified)

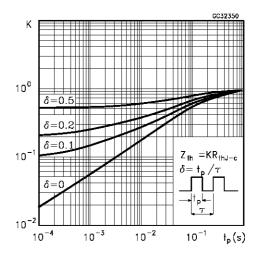
Symbol	Parameter	Test Conditions		Тур.	Max.	Unit	
I _{CES}	Collector Cut-off Current (V _{BE} = 0)	V _{CE} = 1300 V V _{CE} = 1300 V T _j = 125 °C			1 2	mA mA	
I _{EBO}	Emitter Cut-off Current (I _C = 0)	V _{EB} = 5 V			100	μА	
V _{CEO(sus)}	Collector-Emitter Sustaining Voltage	I _C = 100 mA	600			V	
V_{EBO}	Emitter-Base Voltage (I _C = 0)	I _E = 10 mA	10			V	
V _{CE(sat)} *	Collector-Emitter Saturation Voltage	$I_C = 3 \text{ A}$ $I_B = 0.75 \text{ A}$			1.5	V	
$V_{BE(sat)^*}$	Base-Emitter Saturation Voltage	$I_C = 3 \text{ A}$ $I_B = 0.75 \text{ A}$			1.3	V	
h _{FE} *	DC Current Gain	$I_{C} = 3 \text{ A}$ $V_{CE} = 5 \text{ V}$ $I_{C} = 3 \text{ A}$ $V_{CE} = 5 \text{ V}$ $T_{j} = 100 ^{\circ}\text{C}$	5.5 3.5				
t _s	RESISTIVE LOAD Storage Time Fall Time	$V_{CC} = 400 \text{ V}$ $I_{C} = 3 \text{ A}$ $I_{B1} = 0.75 \text{ A}$ $I_{B2} = 1.5 \text{ A}$		1.6 110	2.4 200	μs ns	
t _s t _f	INDUCTIVE LOAD Storage Time Fall Time			3.5 340		μs ns	
t _s t _f	INDUCTIVE LOAD Storage Time Fall Time	$I_{C} = 3 \text{ A}$ $f = 31250 \text{ Hz}$ $I_{B1} = 0.75 \text{ A}$ $I_{B2} = -1.5 \text{ A}$ $V_{ceflyback} = 1200 \sin\left(\frac{\pi}{5} \cdot 10^{6}\right) t$ V		3.5 270		μs ns	

^{*} Pulsed: Pulse duration = 300 μs, duty cycle 1.5 %

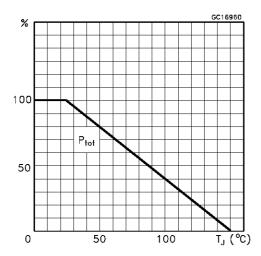
Safe Operating Area



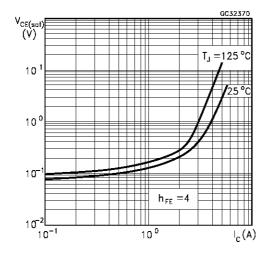
Thermal Impedance



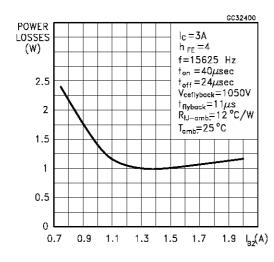
Derating Curve



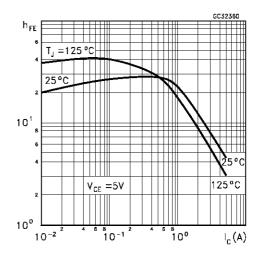
Collector Emitter Saturation Voltage



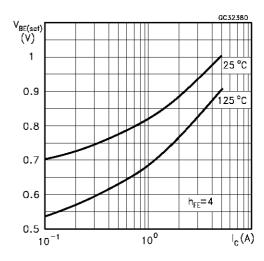
Power Losses at 16 KHz



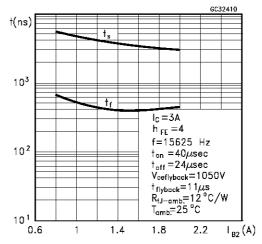
DC Current Gain



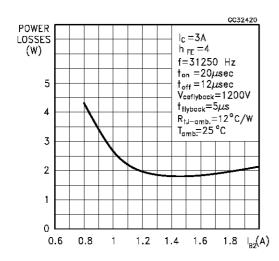
Base Emitter Saturation Voltage



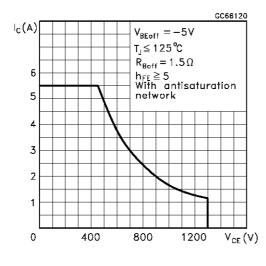
Switching Time Inductive Load at 16KHz (see figure 2)



Power Losses at 32 KHz



Reverse Biased SOA

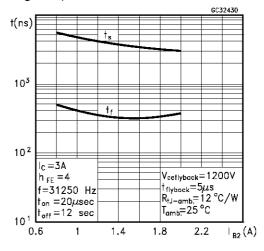


BASE DRIVE INFORMATION

In order to saturate the power switch and reduce conduction losses, adequate direct base current I_{B1} has to be provided for the lowest gain h_{FE} at 100 $^{\circ}$ C (line scan phase). On the other hand, negative base current I_{B2} must be provided to turn off the power transistor (retrace phase).

Most of the dissipation, in the deflection application, occurs at switch-off. Therefore it is essential to determine the value of I_{B2} which minimizes power losses, fall time t_f and, consequently, T_j . A new set of curves have been defined to give total power losses, t_s and t_f as a function of I_{B2} at both 16 KHz, 32 KHz and 64KHz scanning frequencies for choosing the optimum negative drive. The test circuit is

Switching Time Inductive Load at 32 KHz (see figure 2)



illustrated in figure 1.

Inductance L_1 serves to control the slope of the negative base current $l_{\rm B2}$ to recombine the excess carrier in the collector when base current is still present, this would avoid any tailing phenomenon in the collector current.

The values of L and C are calculated from the following equations:

$$\frac{1}{2}L\left(I_{C}\right)^{2} = \frac{1}{2}C\left(V_{CEfly}\right)^{2} \qquad \omega = 2 \pi f = \frac{1}{\sqrt{LC}}$$

Where I_{C} = operating collector current, V_{CEfly} = flyback voltage, f= frequency of oscillation during retrace.

Figure 1: Inductive Load Switching Test Circuits.

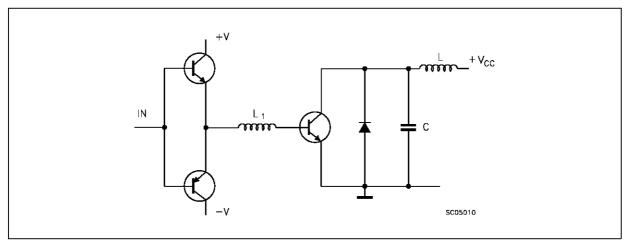
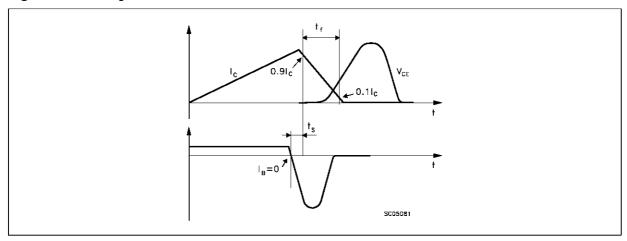
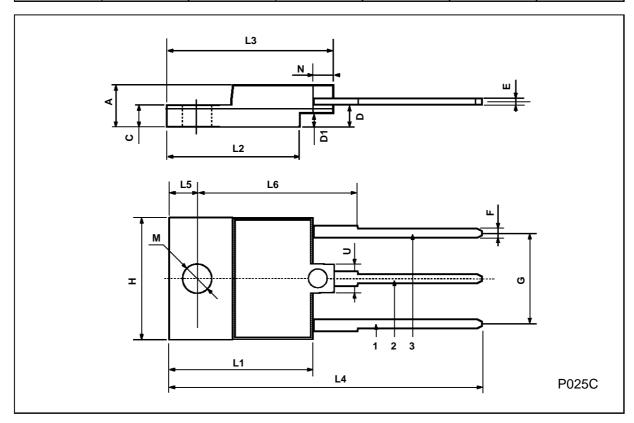


Figure 2: Switching Waveforms in a Deflection Circuit



ISOWATT218 MECHANICAL DATA

DIM.	mm			inch			
DIWI.	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	
А	5.35		5.65	0.210		0.222	
С	3.3		3.8	0.130		0.149	
D	2.9		3.1	0.114		0.122	
D1	1.88		2.08	0.074		0.081	
E	0.45		1	0.017		0.039	
F	1.05		1.25	0.041		0.049	
G	10.8		11.2	0.425		0.441	
Н	15.8		16.2	0.622		0.637	
L1	20.8		21.2	0.818		0.834	
L2	19.1		19.9	0.752		0.783	
L3	22.8		23.6	0.897		0.929	
L4	40.5		42.5	1.594		1.673	
L5	4.85		5.25	0.190		0.206	
L6	20.25		20.75	0.797		0.817	
М	3.5		3.7	0.137		0.145	
N	2.1		2.3	0.082		0.090	
U		4.6			0.181		



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